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Calculation of the Best Date for Transfer Orbit with Perturbation from (GTO) to Lagrange Point (L2)

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Abstract

Lagrange points are points where the gravity of two large celestial bodies does not affect a third body, usually smaller, making its motion follow the motion of the two large bodies. There are five points relative to the Earth, the Sun, and any third body, such as a satellite or a spacecraft. Three essential points are usually symbolized as L1, L2, and L3. This research aims to calculate the best date in 2025 for the satellite to transition from the GTO orbit to the L2 Lagrange point, another transition station to transfer the satellite from (L2) to the Mars orbit. A program was designed in MATLAB to calculate the best date 2025 for the satellite to transition from the Geosynchronous Transfer Orbit (GTO) to the L2 Lagrange point during a transition orbit between the Earth orbit (GTO) to the Sun orbit L2. This requires reaching the escape velocity from the Earth orbit and then the extinction velocity when the spacecraft arrives near L2 in the presence of three types of perturbations: solar gravitational perturbation, the effect of the third body, and the perturbation of the Earth's non-sphericity J2. The results showed that the best date for the transition is Monday, October 2, 2025, because the required velocity for the transition is suitable. The perturbation effect on the orbital elements is small compared to other dates. The transition time is 35.34 days. This means that the departure day will be Monday, Monday, October 2, 2025, and the arrival will be Monday, March 17, 2025. Although there are other dates for the satellite transition with the shortest transition time, the perturbation on the orbital elements of the transition orbit is higher. The perturbation effect on the orbital elements of the transition orbit depends on the satellite's mass. The greater the satellite's mass, the less the effect of perturbation on it, and vice versa.

Keywords: Lagrange points, Geosynchronous Transfer Orbit (GTO), Third body effect, solar attraction.

حساب أفضل تاريخ للمدار الانتقالي مع الاضطراب من (GTO) إلى نقطة لاغرانج (L2)

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الخلاصة

نقاط لاغرانج هي نقاط لا تؤثر فيها جاذبية جسمين سماويين كبيرين على جسم ثالث، عادة ما يكون أصغر، مما يجعل حركته تتبع حركة الجسمين الكبيرين. هناك خمس نقاط بالنسبة للأرض والشمس وأي جسم ثالث، مثل القمر الصناعي أو المركبة الفضائية. عادة ما يرمز إلى ثلاث نقاط أساسية بـ L1 و L2 و L3. يهدف هذا البحث إلى حساب أفضل تاريخ في عام 2025 لانتقال القمر الاصطناعي من مدار GTO إلى نقطة

لاغرانج L2، وهي محطة انتقال أخرى لنقل القمر الاصطناعي من (L2) إلى مدار المريخ. تم تصميم برنامج في MATLAB لحساب أفضل تاريخ 2025 لانتقال القمر الاصطناعي من مدار النقل الجغرافي المتزامن (GTO) إلى نقطة لاغرانج L2 أثناء مدار انتقالي بين مدار الأرض (GTO) إلى مدار الشمس L2. وهذا يتطلب الوصول إلى سرعة الهروب من مدار الأرض ومن ثم سرعة الانقراض عند وصول المركبة الفضائية بالقرب من L2 في وجود ثلاثة أنواع من الاضطرابات: اضطراب الجاذبية الشمسية، وتأثير الجسم الثالث، واضطراب عدم كروية الأرض L2. وأظهرت النتائج أن أفضل موعد للانتقال هو يوم الاثنين 2 أكتوبر 2025، لأن السرعة المطلوبة للانتقال مناسبة. وتأثير الاضطراب على العناصر المدارية صغير مقارنة بالتواريخ الأخرى. وزمن الانتقال هو 35.34 يوماً. وهذا يعني أن يوم المغادرة سيكون يوم الاثنين 2 أكتوبر 2025، وسيكون يوم الوصول يوم الاثنين 17 مارس 2025. وعلى الرغم من وجود تواريخ أخرى لانتقال القمر الاصطناعي بأقصر زمن انتقال، إلا أن الاضطراب على العناصر المدارية لمدار الانتقال أعلى. ويعتمد تأثير الاضطراب على العناصر المدارية لمدار الانتقال على كتلة القمر الاصطناعي. كلما زادت كتلة القمر الاصطناعي، كلما كان تأثير الاضطراب عليه أقل، والعكس صحيح.

1. Introduction:

Lagrange points are points in space where transmitting objects, like satellites, tend to remain stationary. At Lagrange points, the centripetal force of a tiny body traveling alongside two massive mass bodies equals the gravitational force. Figure 1 shows the Lagrange points, which satellites use to lower the fuel needed to maintain their position in space.

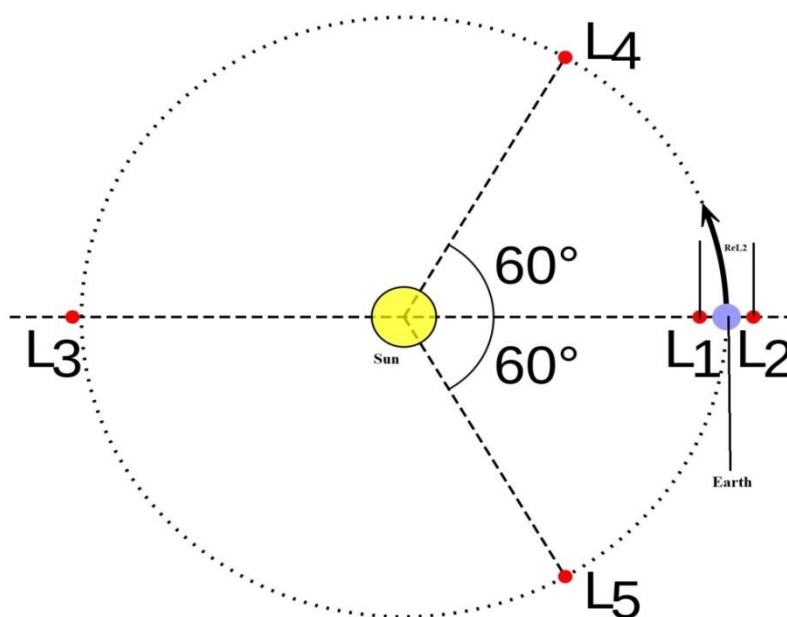


Figure 1: The Lagrange points of Earth's orbits relative to the Sun [1].

Since the Earth is a solar system, all planets and other components are primarily under the influence of the sun's gravity. However, there is another effective force acting on the Earth, like the moon and other planets, proportional to their mass and distance from the Earth, to study these cases mathematical equations for gravitational effect upon the mentioned body under study. The need for space exploration and satellite and space telescope technology led to the study of the optimum place for these space tools around Earth orbital. Several physics and classical mechanics methods were introduced to examine these places, such as two-body (in 1609, the two-body problem was analyzed by Johannes Kepler and solved by Isaac Newton in 1687). The three-body problem, which is the problem of taking the initial velocities and

positions (or momenta) of three-point masses and solving for their motion following Newton's laws of motion and Newton's law of universal gravitation, is the more straightforward and realistic case in which the three body problem was studied [1]. One particular instance of the n-body problem is the three-body problem. In the past, the Earth, Sun, and Moon three-body problem was the first particular three-body problem to be thoroughly studied [2]. To find the differential equations that would account for the motion of the bodies, Newton initially investigated the concept in 1687. Although numerous other researchers have investigated the issue, Poincare's seminal work in 1890 marked a significant advancement [3]. There are typically 18 first-order differential equations in a three-body problem. It can be whittled down to 6 using maths and conservation equations. Because there aren't enough conservation quantities to support further simplification, the problem hasn't been addressed yet. Looking at more limited examples to understand what would happen in constrained situations is best. Two massive masses orbit their shared center of mass in a circle in the restricted three-body problem. There is the entry of a third body into the system, which is considerably smaller than the other two. The challenge is determining how this object will move as it is affected by the gravitational pull of the larger bodies. The circular restricted three-body issue applies to many circumstances in the solar system. The eccentricity of the Earth's orbit around the Sun is 0.0167, and the Moon's orbit around Earth is 0.0516; the old dates make their orbits essentially circular [4].

Previous research and studies on this topic focused on geostationary orbit (GEO), medium Earth orbit (MEO), and low Earth orbit (LEO) satellites, such as GPS and GLONAS, which were studied by Sue in 2000 [5]. The effects of atmospheric drag and zonal Harmonics on the orbits of satellites in low Earth orbit is a study by Al-Burmani and S. Barron (2009), which concluded that there is no apparent effect of the J2 spherical harmonics of the gravitational potential during the early stage of injection. The dominant effect was the drag force in the atmosphere at the perigee, which decreased the satellite's altitude until its return after 1560 days in a dense atmosphere [6]. In the year (2017) Allam, Awad, and Amin calculated the Bi-Elliptic Hohmann transfer and one tangent burn transfer calculations using Monte Carlo simulation. In 2020, Mahdi, Saleh, and Jarad studied determination and published an article whose main objective was to evaluate the orbital transition methods between two elliptical earth orbits.

The U.S. National Aeronautics and Space Administration (NASA) led Webb's design and development and partnered with two central agencies: the European Space Agency (ESA) and the Canadian Space Agency (CSA). The NASA Goddard Space Flight Center in Maryland managed telescope development, while the Space Telescope Science Institute in Baltimore on the Homewood Campus of Johns Hopkins University operates Webb. The primary contractor for the project was Northrop Grumman. He Webb was launched on 25 December 2021 on an Ariane 5 rocket from Kourou, French Guiana. In January 2022, it arrived at its destination, a solar orbit near the Sun-Earth L2 Lagrange point, about 1.5 million kilometers (930,000 mi) from Earth. The telescope's first image was released on 11 July 2022. The telescope is named after James E. Webb, who was the administrator of NASA from 1961 to 1968 during the Mercury, Gemini, and Apollo programs [7].

The importance of this research is that having a project to transfer a satellite from Earth to Mars, and this research is one of the steps to transition to L2 because it is low voltage and through which the transfer to Mars is done, and expect that the energy difference in this method will be less than direct transfer.

In this research, the Hohmann method was used for transition. The Hohmann transfer method is an elliptical orbit that contacts both inner and outer orbits, and the transfer orbit from

the perigee or apogee of the initial orbit to the final orbit is direct in half a period. The Hohmann transfer methods have different efficiency for two-impulse maneuvers and depend on the height of the initial orbit.

Table 1: Types of satellites (space telescopes) that reached Lagrange points

Satellites Lagrange points EARTH/SUN	Date	L1	L2	L3	L4	L5
SOHO (Solar and Hemispheric Observatory)	1995	••				
ACE (Advanced Composition Explorer) space-borne energetic particles from the Sun-Earth	1997	••				
DSCOVR (Deep Space Climate Observatory) is an American space weather station that monitors changes in the solar wind, providing space weather alerts and forecasts for geomagnetic storms.	1998	••				
WMAP(The Wilkinson Microwave Anisotropy Probe) to make the fundamental measurements of cosmology, the study of the properties of our universe as a whole	2001		••			
GENESIS(probe that collected a sample of solar wind particles and returned them to Earth for analysis)	2001	••				
PLANCK(study the Cosmic Microwave Background)	2009		••			
HERSCHEL(the only space observatory that covered the spectral range from far-infrared to sub-millimeter Wavelengths)	2009		••			
GAIA(Space Observatory (ESA) the spacecraft is designed for astrometry: measuring the positions, distances, and motions of stars with unprecedented precision and the positions of exoplanets by measuring attributes about the stars they orbit, such as their apparent magnitude and color)	2013		••			
JWST(James Webb Space Telescope)	2022		••			

The gravitational three-body problem is a special case of the circular restricted gravitational three-body Circular Restricted Gravitational Three-Body Problem (CRGTBP).

The n-body problem: The CRGTBP consists of three bodies; these two bodies (which are named the primaries or the primary and the secondary) move in a circular orbit about their center of mass's center influenced by gravitation between them with the infinitesimal mass body, which the third body move under their gravitational effect of the two masses where its mass could be negligent influence compared these two masses. Moreover, the common plane movement of the body is defined by both the primary and secondary [8][9][10].

The two larger bodies' masses are denoted as m_1 and m_2 , and they are assumed to be traveling in a circle with a radius of r_{12} around each other under the influence of only their mutual gravitation. Consider a non-inertial, co-moving frame of reference (x, y,z) originating at the two-body system's center of mass (G); the z-axis is perpendicular to the orbital plane where the y-axis is located. m_1 and m_2 appear to be at rest in this frame of reference, as shown in Figure (2), where the constant inirtial angular velocity Ω is provided by [11].

$$= \sqrt{\mu/(r_{12})^3} \quad (1)$$

Since M is the total mass of the system, $M = m_1 + m_2$, $\mu_e = GM_e$, r_{12} is distance between m_1 and m_2

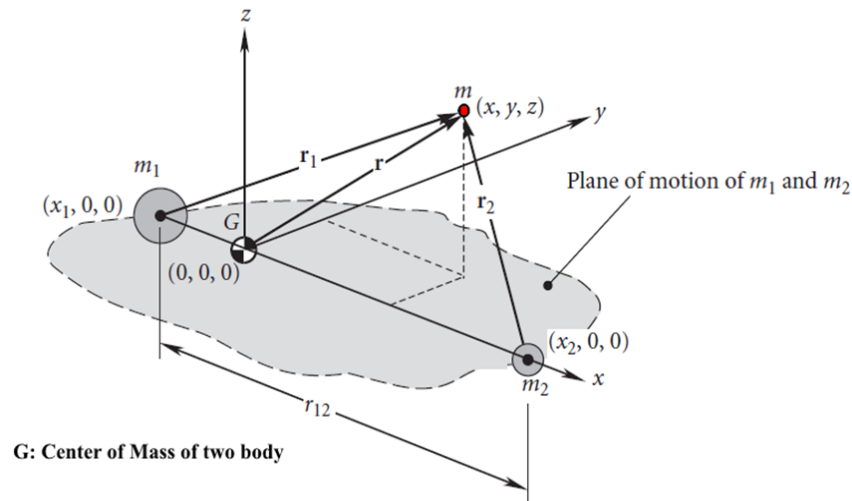


Figure 2: m_1 and m_2 are the two primary bodies that revolve around each other in a circular orbit, in addition to a secondary mass, m [11].

From the definition of the center of mass, the dimensionless mass ratios are given by

$$\begin{aligned} \pi_1 &= m_1/M, \quad \pi_2 \\ &= m_2/M \end{aligned} \quad (2)$$

π_1 and π_2 represents the center of mass

This is known as the circular restricted three-body problem Circular Restricted Gravitational Three-Body Problem (CRGTBP) because the mass m is assumed to be so small that it does not affect the motion of the primary bodies. It introduces a third body of mass, m , which is vanishingly small compared to the primary mass. m_1 and m_2 , like the mass of a spacecraft compared to that of a planet or moon in the solar system.

The secondary mass m location vector concerning m_1 is provided by [11].

$$r_1 = (x - x_1)\hat{i} + y\hat{j} + z\hat{k} = (x + \pi_2 r_{12})\hat{i} + y\hat{j} + z\hat{k} \quad (3)$$

About m_2 the location vector of the secondary mass m is [11].

$$r_2 = (x - \pi_1 r_{12})\hat{i} + y\hat{j} + z\hat{k} \quad (4)$$

The position vector of the secondary body relative to the center of mass is [11].

$$r = x\hat{i} + y\hat{j} + z\hat{k} \quad (5)$$

Let us observe that Newton's second law for the secondary body is

$$m\ddot{r} = F_1 + F_2 \quad (6)$$

F_1 and F_2 are the gravitational forces exerted on m_1 and m_2 , respectively.

$$F_1 = -(Gm_1 * m)/(r_1)^3 * r_1$$

$$F_2 = -(Gm_2 * m)/(r_2)^3 * r_2$$

$$\text{If } \mu_1 = Gm_1, \quad \mu_2 = Gm_2$$

By substituting in equation (6), the acceleration relation is obtained.

$$\ddot{r} = -\mu_1/(r_1)^3 * r_1 - \mu_2/(r_2)^3 * r_2 \quad (7)$$

By substitute the inertial angular velocity and the position vectors in acceleration relation and by arranging the variables components and equating the coefficients of \hat{i} , \hat{j} and \hat{k} on each side of this equation yields the three scalar equations of motion for the circular restricted three-body problem [11].

$$\ddot{x} - 2\Omega\dot{y} - \Omega^2 x = -\mu_1/(r_1)^3 (x + \pi_2 * r_{12}) - \mu_2/(r_2)^3 (x + \pi_1 r_{12}) \quad (8-a)$$

$$\ddot{y} + 2\Omega\dot{x} - \Omega^2 y = \mu_1/(r_1)^3 y - \mu_2/(r_2)^3 y \quad (8-b)$$

$$\ddot{z} = -\mu_1/(r_1)^3 z - \mu_2/(r_2)^3 z \quad (8-c)$$

2- Methodology:

L2 will be included in our primary calculations since it is perfect for astronomy since a spacecraft can easily connect with Earth, maintain the Sun, Earth, and Moon behind the spacecraft for solar power, and give our telescopes a clear view of outer space.

Earth's orbit and the L2 point have an ellipse orbit around the Sun. Then, the distance and velocity are derived from the equation of motion, which is not exact because of the effect of other bodies (such as planets) on Earth.

The distance between the Sun and Earth at a given location in its orbit (during the year) R_{ES} , orbital equation was used [11].

$$R_{ES} = \frac{a_e(1-e_e^2)}{(1+e \cos \theta)} \quad (9)$$

Where a_e , e_e and θ represent the semi-major axis, eccentricity, and true anomaly of the Earth's orbit around the Sun.

On the other hand, the orbital velocity of the Lagrange points (L2) around the Sun was calculated using the orbital velocity equation [12].

$$V_L = \sqrt{\mu \left(\frac{2}{R_{EL2}} - \frac{1}{a_{L2}} \right)} \quad (10)$$

Where μ_{\odot} represent GM_{\odot} and R_{EL2} is the instantaneous distance from the Sun, which is calculated by adding R_{ES} and Lagrange points distance from Earth at time.

Another method was used to calculate the orbital velocity of the (L) using Newton's law of gravity.

$$\frac{M_{EG}}{R_{EL}^2} + \frac{M_{\odot G}}{R_{SL}^2} = \frac{V_{Or}^2}{R_{SL}} \quad (11)$$

Where V_{Or} , R_{EL} and R_{SL} represent the orbital velocity of the Lagrange point on its orbit around the Sun, the distances between the Earth and Lagrange point (L2), and the Sun and Lagrange point L2.

The following is the perturbed Equation of Motion (EOM) on the perturbed elliptical orbit [13]:

$\ddot{\mathbf{r}} = \frac{d^2\mathbf{r}}{dt^2}$ is the satellite acceleration at the time (t) in unit km/s^2 .

$$\ddot{\mathbf{r}} = -\frac{\mu}{r^3} \vec{r} + \ddot{\mathbf{r}}_p \quad (12)$$

Where $\mu_e = G * M_e = 398603.4416$ when the distance in km and the time in sec where G is the gravitational constant and M_e is the Earth mass, \vec{r} is the position vector for the satellite, and r is the distance between the earth's center and satellite at time (t) [11].

Where $\ddot{\mathbf{r}}_p$ is the perturbation acceleration, which can be written as the following

$$\ddot{\mathbf{r}}_p = \ddot{\mathbf{r}}_E + \ddot{\mathbf{r}}_S + \ddot{\mathbf{r}}_M + \ddot{\mathbf{r}}_{sp} + \ddot{\mathbf{r}}_A \quad (13)$$

Where $\ddot{\mathbf{r}}_E$ is the non-spherically and inhomogeneous mass distribution within Earth (central body), $\ddot{\mathbf{r}}_S$ and $\ddot{\mathbf{r}}_M$ is the Sun and the Moon acceleration attraction on the satellite, $\ddot{\mathbf{r}}_{sp}$ acceleration due to Solar radiation pressure and $\ddot{\mathbf{r}}_A$ acceleration due to atmospheric drag.

Two types of perturbations were used in this study (solar attraction, third body effect, and non-spherical Earth orbit J2) [14].

The solution of the equation (12) is give the satellite distance [15]:

$$r = \frac{h^2}{\mu} \frac{1}{1+e \cos(f)} \quad (14)$$

h: angular momentum per unit mass f: True anomaly angle (0,360°).

From equation (3), the perigee and apogee distance r_p , r_a are derived at $f=0$ and 180 degrees.

$$r_p = a(1-e) \quad (15A)$$

$$r_a = a(1+e) \quad (15B)$$

Where a is the semi-major axis of the elliptical orbit.

The eccentricity of the transfer orbit can be calculated by [15]:

$$e = \frac{r_a - r_p}{r_a + r_p} \quad (16)$$

Where r_a : is the distance between L2 and the Earth upon arrival time.

r_p : is the distance of the satellite from the Earth center at the start of the transition.

This equation was used to calculate the angular momentum [15].

$$h = \sqrt{2\mu} \frac{\sqrt{r_a - r_p}}{\sqrt{r_a + r_p}} \quad (17)$$

This equation calculates the velocity for an elliptical orbit [15].

$$v^2 = \mu \left(\frac{2}{r} - \frac{1}{a} \right) \quad (18)$$

The semi-major axis (a) can be calculated from equation (15A or 15B) [15].

The following equation may be used to determine the velocity needed to transfer the satellite from its initial orbit to its final orbit through the transition orbit. The change in velocity required to transition is represented by the symbol Δv [16].

Then, transition time is required. Equation (10) can be used to get the transition time where $\mu=398602.4415$ at a, r in km, and the period in second, $T_{trans}=1/2T$.

$$T_{tran} = \frac{1}{2} \left(\frac{2\pi}{\sqrt{\mu}} a^{\frac{3}{2}} \right) \quad (19)$$

The mass of a satellite is not constant through transition orbit because of mass burn. This can be written as the following [15]:

$$\frac{\Delta m}{m} = 1 - e^{-\frac{\Delta v}{Isp g_0}} \quad (20)$$

Where:

Δm is the consumed mass for propellant, g_0 is the gravity standard of acceleration, and Isp is the impulsive specific of the propellants. The vectors perturbation accelerations on satellite is given as the following [17] [18]:

$$a_{J2} = \frac{-3\mu R_e^2 J_2}{2r^7} \begin{bmatrix} x(x^2 + y^2 - 4z^2) \\ y(x^2 + y^2 - 4z^2) \\ z(3x^2 + 3y^2 - 2z^2) \end{bmatrix} \quad (21)$$

Where (R_e) is the Earth radius (6372 km) and ($x, y, and z$) are the components of the satellite position, r is the distance of the satellite. The J_2 value for Earth is $J_2=1082.6283 \times 10^{-6}$.

4. Result and Discussion:

The MATLAB program designed a program to calculate the orbital elements of the primary and transitional orbit and the effect of disturbance on the orbital elements of the transitional orbit. The perturbed equation was solved using the 4th-order Runge–Kutta method. The most commonly used Runge-Kutta method to find the solution of a differential equation is the RK4 method, i.e., the fourth-order Runge-Kutta method. The Runge-Kutta method provides the approximate y value for a given point x . Only the first-order ODEs can be solved using the Runge Kutta RK4 method. (It is one of the integration methods to calculate velocity from acceleration or distance from velocity. It uses six values of the variable that are predicted by exchanging the function in the previous period [18][19][20].

Algorithm:

1. Calculated the (JD).
2. Calculate the Geocentric coordinates of the sun through the year.
3. Calculate the heliocentric coordinates of the Earth and L2 through one year.
4. Calculate the orbital element of the initial satellite orbit around the Earth.
5. Calculate the energy required Δv total, $T_{\text{transition}}$, $\Delta m/m$, for the transfer orbit from the orbit around the Earth to the orbit of L2 around the Sun.
6. Calculate orbital elements of transfer orbit with perturbations.
7. Calculate the best transfer orbit by changing the date of the start of the transfer.

These results, gated by equations (1,2,6,8,9,10,12,14,15A,15B,16,17,18,19,20,21), were written in Table (2). The change in the orbital elements of the transition orbit in the presence of perturbations shows these results for half a cycle, where it becomes clear to us that the orbital element most affected by perturbation is the semi-major axis, Figures (3, 4, 5, 6, 7, 8, 9, and 10). Each drawing represents a specific date and month for 2025 and the extent of the influence of the perturbations. The results showed that the best date for the transition is Monday, February 10, 2025, because the velocity required for the transition is appropriate, its small value about (Δv total = 4.17897268314359 km/s), which is the sum of the delta-v in the velocity required to transition from the GTO orbit and delta- V_2 , which is it represents the velocity that the satellite needs to brake and reduce its velocity when arriving near the Lagrange L2. The effect of the perturbation on the orbital elements is also tiny compared to the other dates. The time for transition is 35.3426225316822 days. This means the departure day will be Monday, February 10, 2025, and arrive on Monday, March 17, 2025. Although there are other dates to transition satellites in the shortest time of transition, the perturbation on the orbital elements of the transition orbit is high; for example, 10/3/2025 and 10/9/2025 need the time transition of about 32 days, but the perturbation is high the second result can be used if it is not possible to transition on the first date for technical reasons, for example.

Figure (11) shows the greatest effect of the perturbation on the inclination of the transfer orbit on 10/4/2025 and also on 10/10/2025 and the low value in inclination on 10/6/2025. As for its effect on the semi-major axis, it peaks on 10/6/2025. The reason for this is the influence of the third body, for example, the Moon and that effect will change due to a location change in the moon with the date, Figure (12). Figure (13) shows the omega angle effect by perturbation reached a higher value on 10/10/2025 and 10/4/2025; the true Anomaly's highest value is due to the perturbation effect on 9/10/2025, Figure (14). As for the Right Ascension of ascending node, it reaches its highest value on 12/10/2025 and its lowest value on 11/10/2025 in Figure (15). Eccentricity is the last element affected by the perturbation, with the highest value on April 10, 2025, Figure (16).

Table 2: The variation orbital elements of the transition orbit with different dates of starting the transfer.

date	Δi (deg)	Δa (k m)	Δta (deg)	$\Delta \Omega$ (deg)	$\Delta R.A$ (deg)	Δe	T_{tran} (day)	Δv - total (km/se c)	$\Delta m/m$
10/1/2025	- 0.0965700 46116	36643. 26	0.2839	- 0.5874572 485546	31.5766 6506	- 0.0385564 25	43.721 0222	4.1960 8603	0.35134
10/2/2025	- 0.1436690 24351	18424. 71	3.0578 75642	0.3999794 3486	30.1541 9824	- 0.0525257 4	35.342 6225	4.1789 7268	0.35134
10/3/2025	- 0.3611720 48473	37229. 23	4.3335 10329	1.0800905 96497	30.0276 1118	- 0.0357364 57	32.513 8103	4.5524 7793	0.35134
10/4/2025	- 0.4154923 99989	14079. 23	2.5402 32367	1.1597345 76696	30.1620 5554	- 0.0274254 28	34.633 4693	4.6483 5892	0.35134
10/5/2025	- 0.1966663 56264	40388. 27	3.1537 38258	0.2310957 582995	29.7351 3856	- 0.0606164 5609	42.653 9720	3.8914 8699	0.35134
10/6/2025	- 0.0863437 9043	72080. 42	2.6968 9648	- 0.9032896 653568	31.2002 2590	- 0.0523367 1454	50.381 3008	3.8577 0463	0.35134
10/7/2025	- 0.1050899 77225	40122. 42	1.0701 79645	- 0.6679581 826523	31.6229 3744	- 0.0388527 0303	44.579 1399	4.1722 8050	0.35134
10/8/2025	- 0.0982317 14265	11003. 30	0.1358 37128	0.2425717 326471	30.4059 1684	- 0.0496891 4239	36.370 1839	4.1949 8911	0.35134
10/9/2025	- 0.3434088 23610	36409. 34	5.1677 06593	1.0503826 18218	29.9243 4273	- 0.0394525 2307	32.535 6074	4.4820 9822	0.35134
10/10/2025	- 0.4309635 14856	18903. 51	1.9311 18037	1.2209234 28410	29.8186 1180	- 0.0343404 7668	34.028 8434	4.5296 6363	0.35134
10/11/2025	- 0.2096365 81771	41315. 07	1.7513 06157	0.2027945 633050	29.7333 7039	- 0.0609501 5052	39.162 2832	3.8768 2079	0.35134
10/12/2025	- 0.1005160 43388	78646. 20	0.4098 95866	- 1.0230190 20900	31.9237 9582	- 0.0356008 6204	52.074 7522	4.0782 7249	0.35134

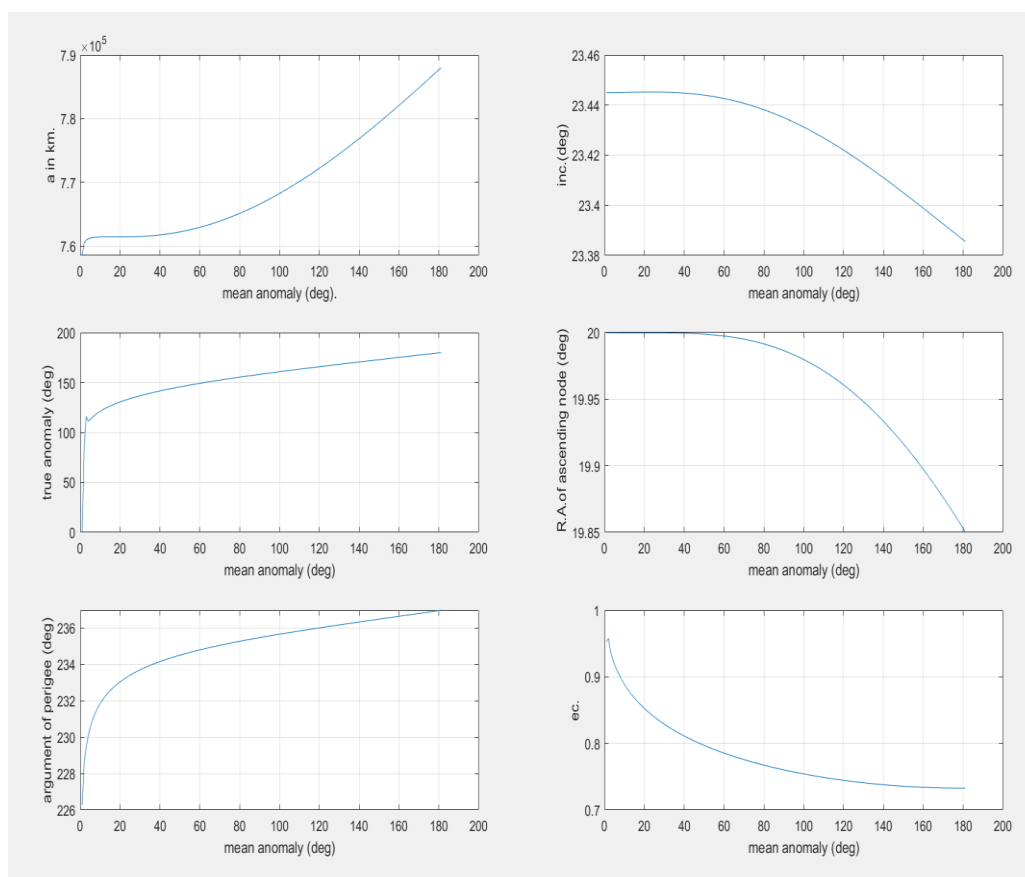


Figure 3: The variation orbital elements of the transition orbit on 10/1/2025.

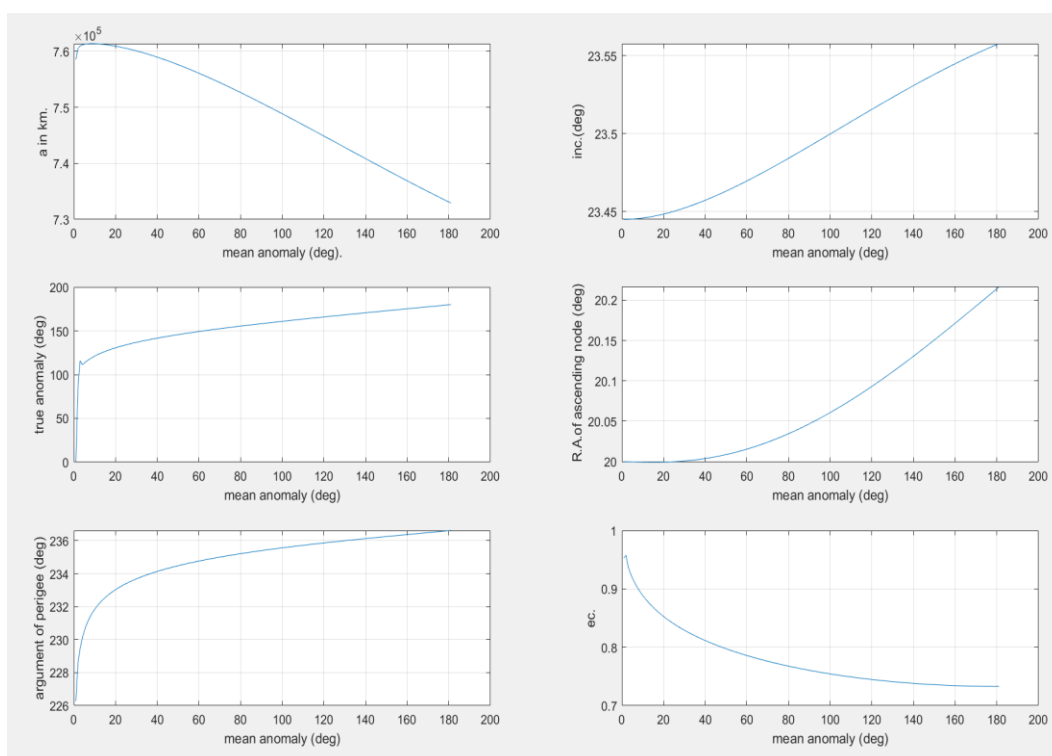


Figure 4: The variation orbital elements of the transition orbit in 10/2/2025

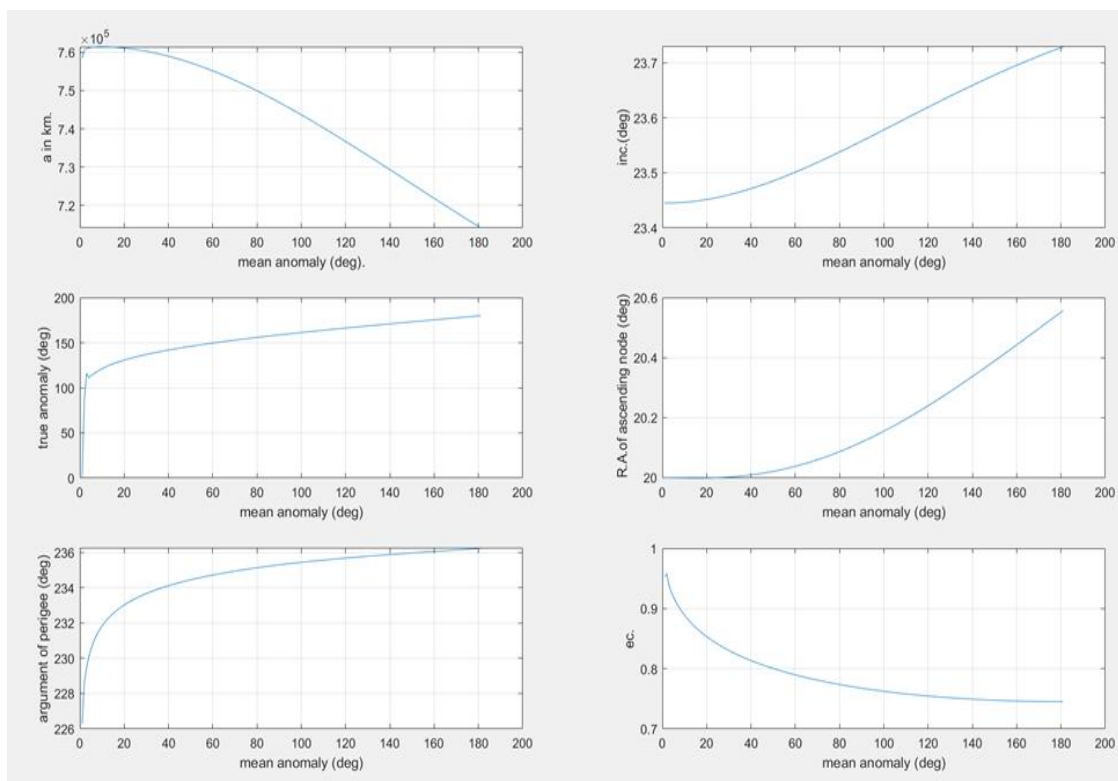


Figure 5: The variation orbital elements of the transition orbit in 10/3/2025

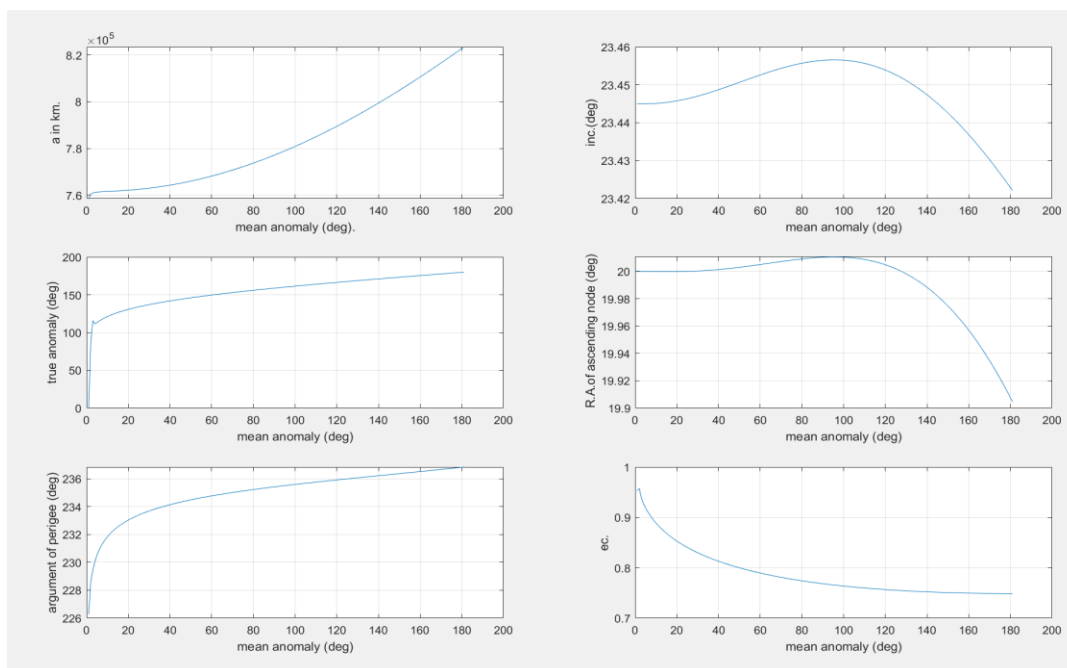


Figure 6: The variation orbital elements of the transition orbit on 10/6/2025

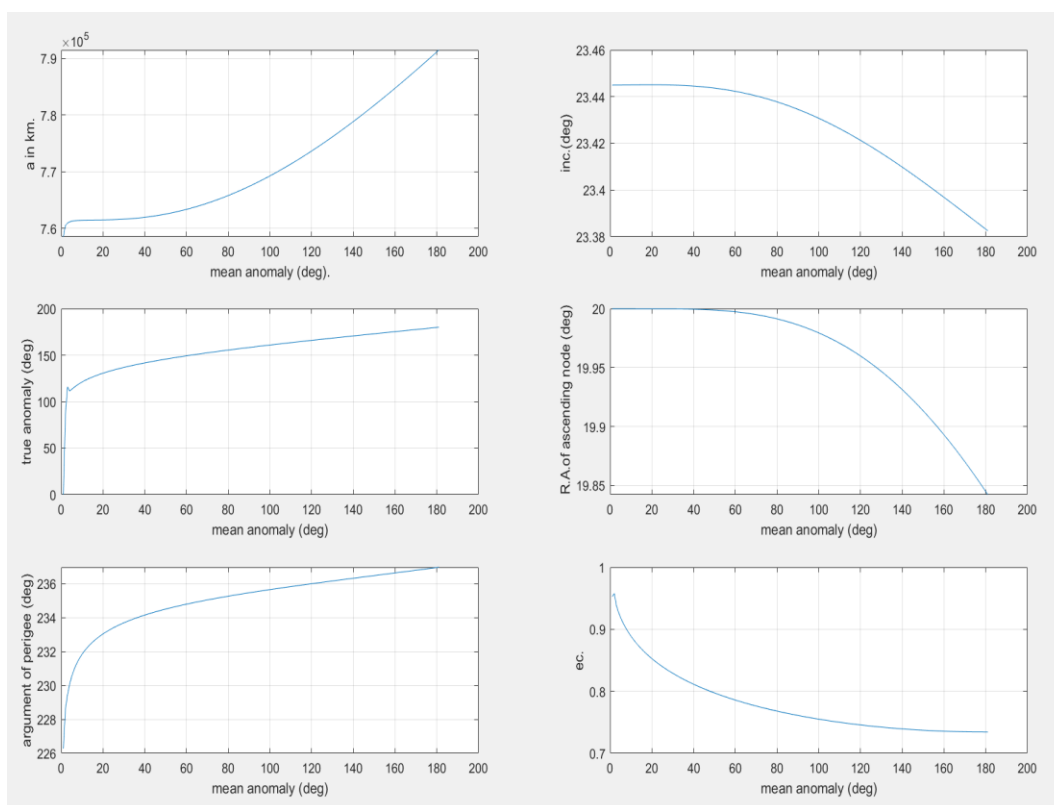


Figure 7: The variation orbital elements of the transition orbit on 10/7/2025

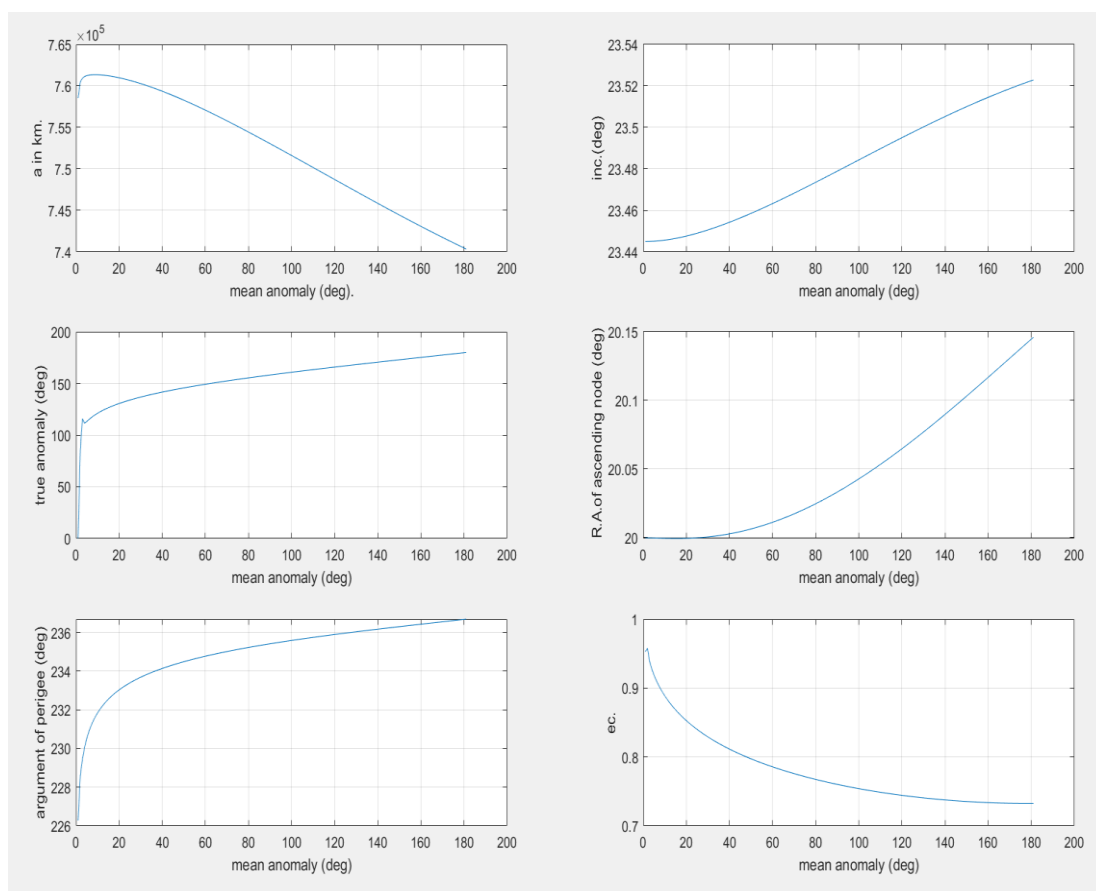


Figure 8: The variation orbital elements of the transition orbit on 10/8/2025

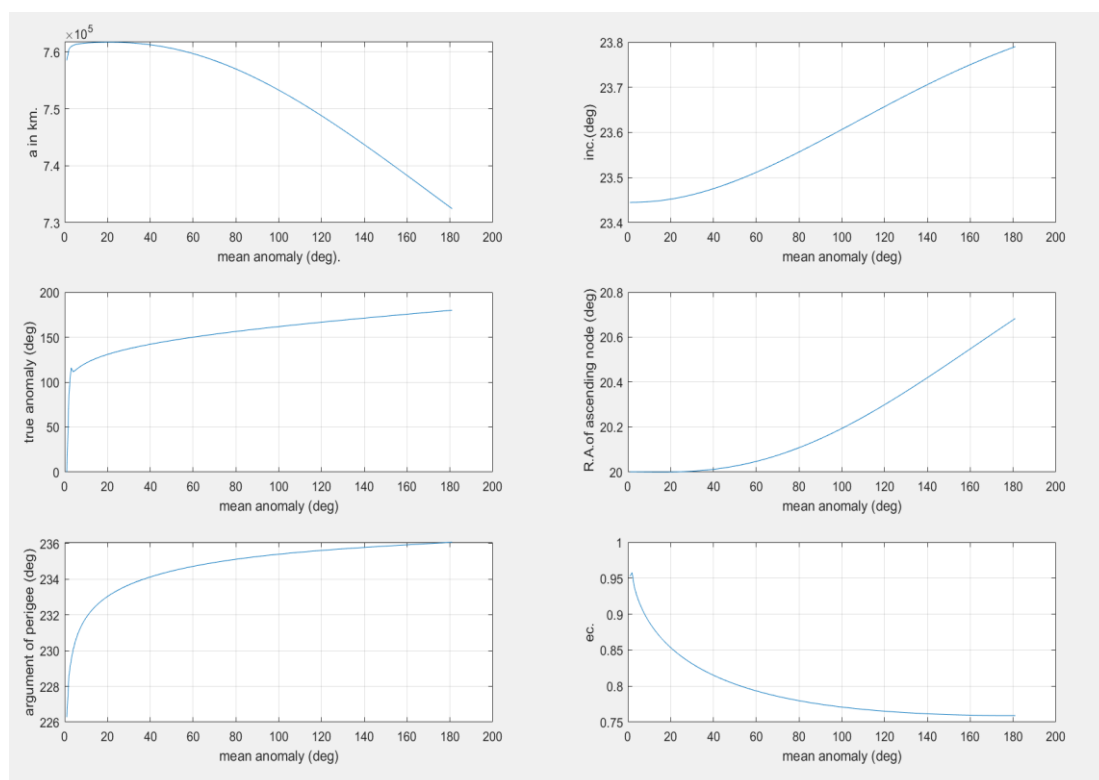


Figure 9: The variation orbital elements of the transition orbit on 10/10/2025

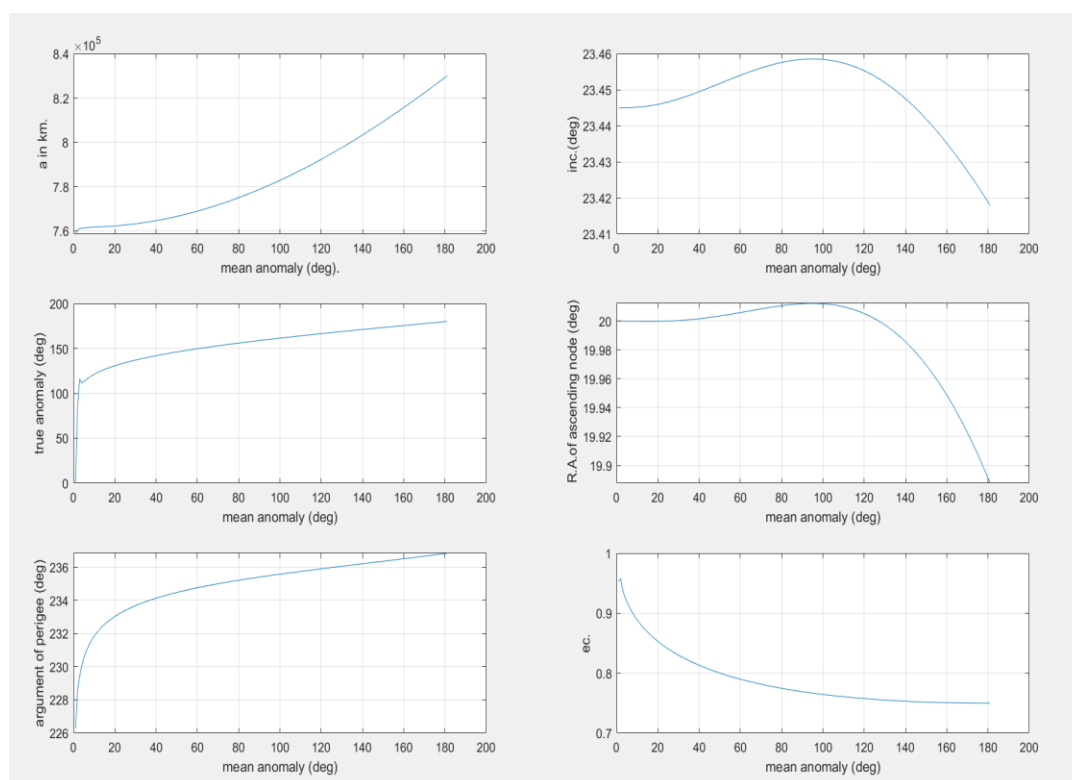


Figure 10: The variation orbital elements of the transition orbit on 10/12/2025

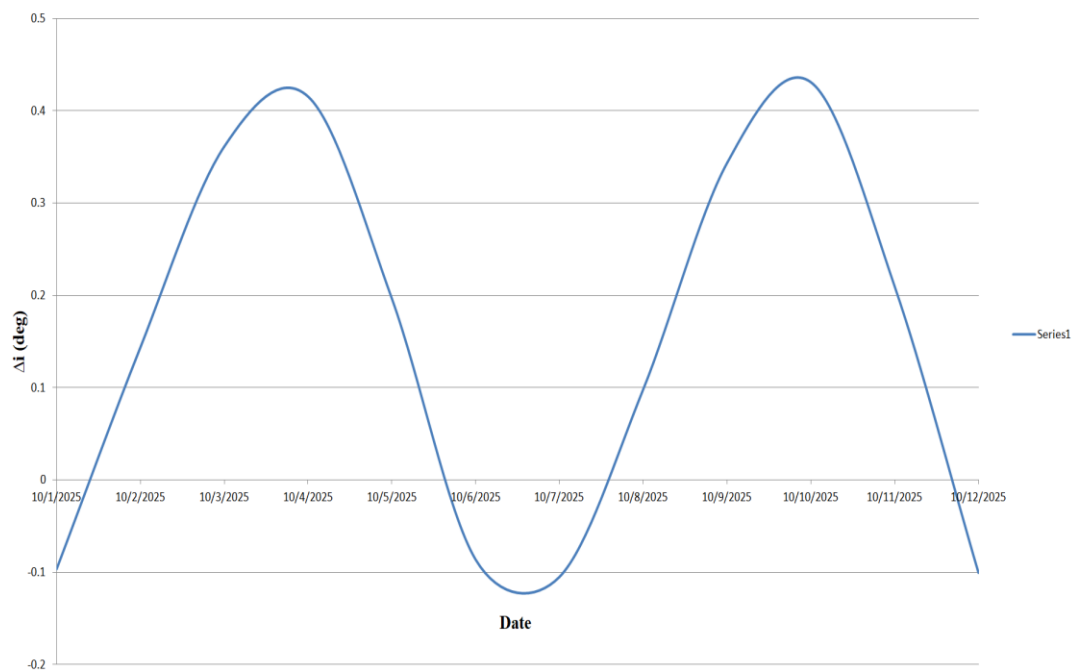


Figure 11: The variation inclination of the transition orbit with date

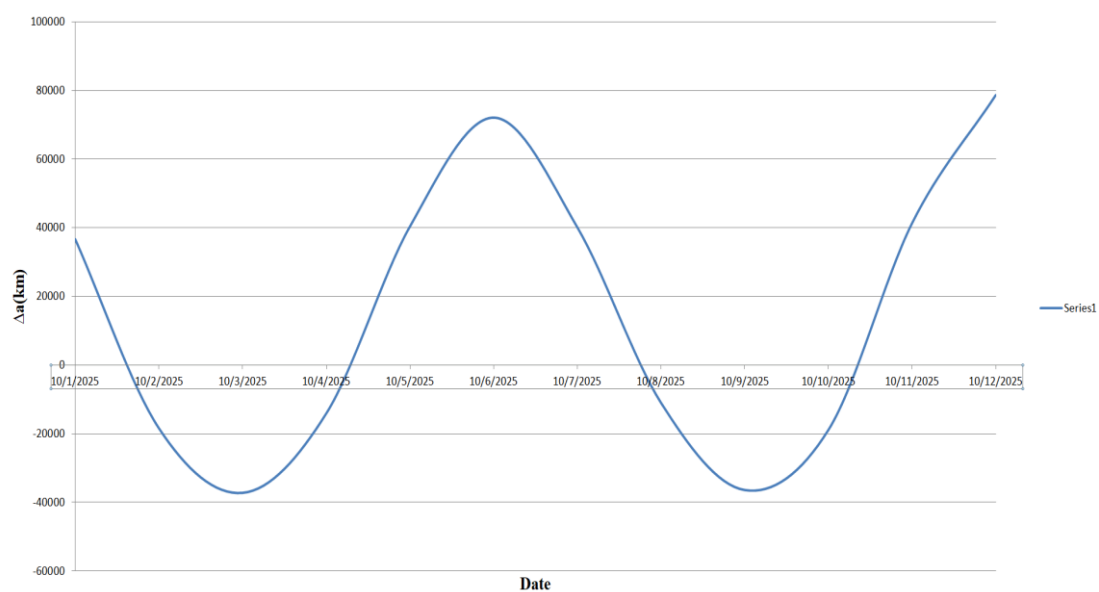


Figure 12: The variation semi-major axis of the transition orbit with the date

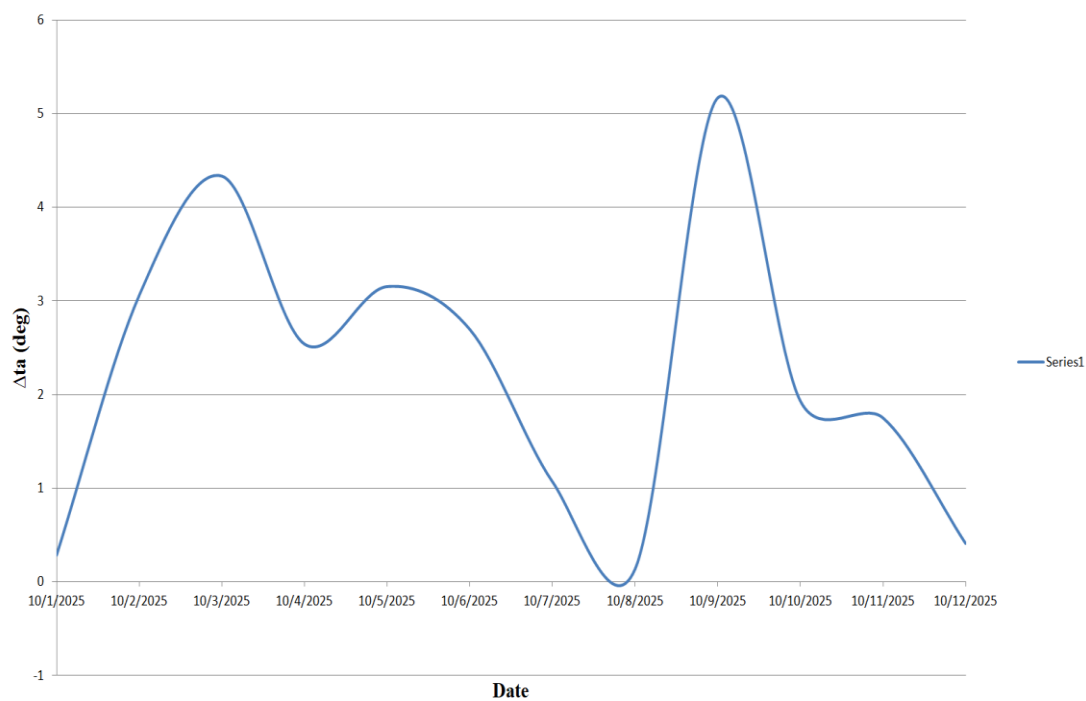


Figure 13: The variation true anomaly of the transition orbit with date

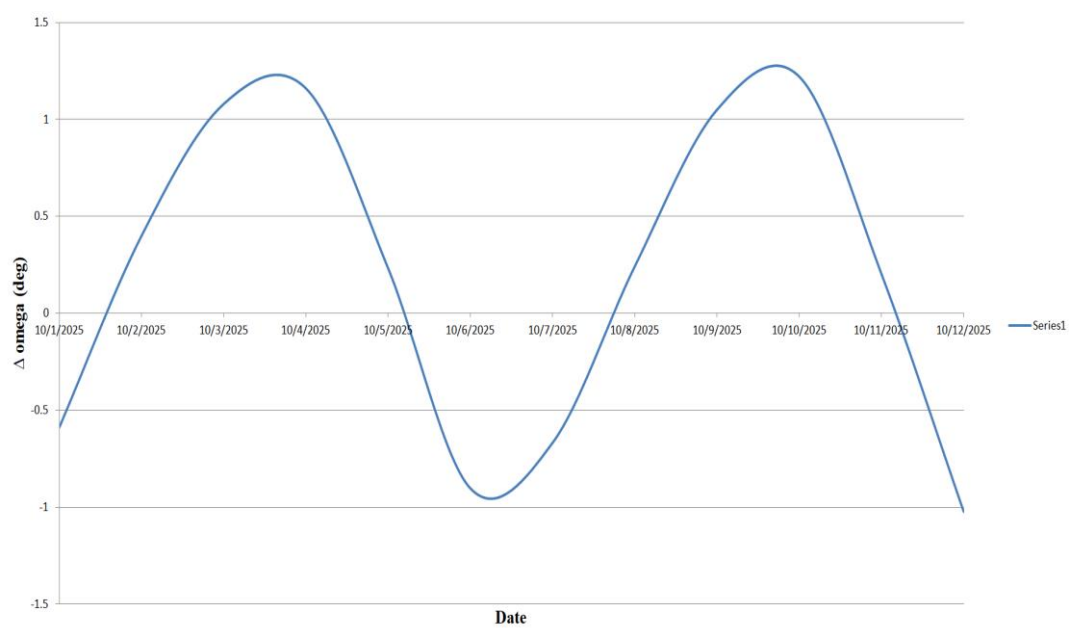


Figure 14: The variation omega of the transition orbit with date

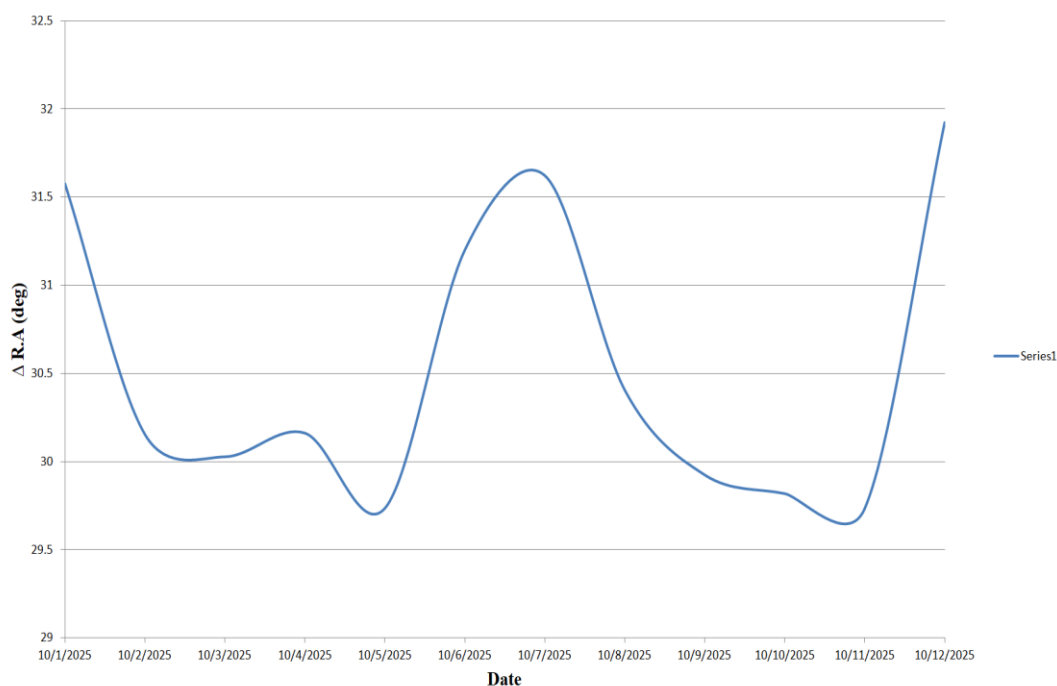


Figure 15: The variation R.A of the transition orbit with date

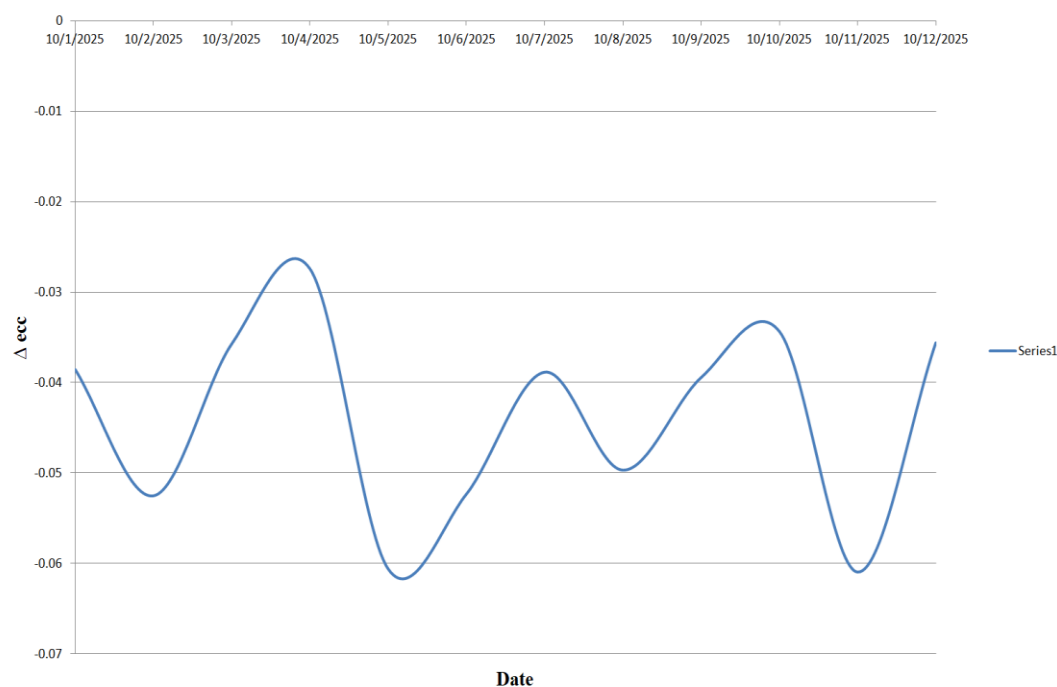


Figure 16: The variation eccentricity of the transition orbit with date

5-Conclusions:

In this research, several things were concluded:

The type of perturbation most affecting the orbital elements is the third-body effect, and the effect of perturbation increases with the mass of the satellite. It concludes that the best day to transition from GTO to Lagrange point L2 was chosen: February 10, 2025. The reason is that the impact of the perturbation is low compared to other dates, and the velocity required for the transition ΔV_1 and the braking velocity ΔV_2 are appropriate; the perturbations' effect on the transition orbit's orbital elements is small. Its effect is clear on the semi-major axis but cannot be neglected. The reason is the cumulative value. If the transition does not take place during

one cycle, its effect may be very clear; the advantage of studying the L2 is home to some of the most extraordinary space missions where the latest satellite to reach L2 is the James Webb Space Telescope (launched on 25 December 2021) and for any space station for starting point mission is to study nearby explants and explore the farthest reaches of the Universe to observe the very first galaxies, It is important to refer that calculation were done are approximately because its canceled the gravitational effect of planets and moon for simplicity.

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